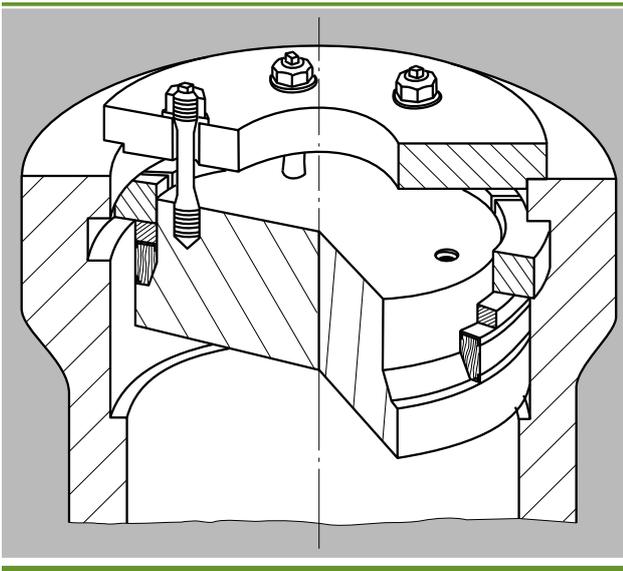


## Cover plate gaskets

Cover plate gaskets are used as self-sealing gaskets, meaning that the sealing force does not come from bolts but from the internal pressure. Therefore bolts with a smaller cross-section can be selected. The entire connection is more compact. The following illustration shows the design principle.

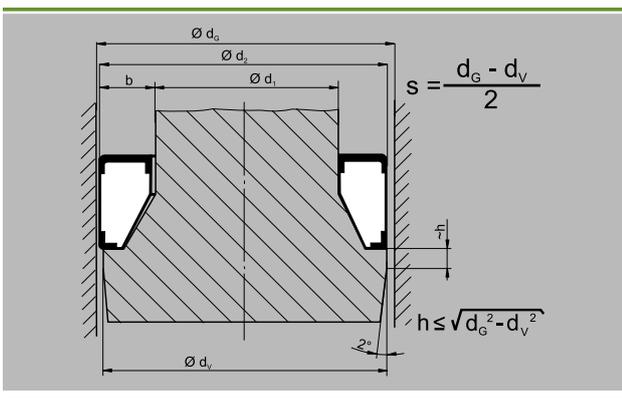


At high pressures or with reworked covers, caps should be provided, so that the graphite does not extrude into the gap between the housing and the cover plate. Compressed caps are made of 0.4 mm thick stainless steel sheet metal 1.4541. At very high pressures solid, lathed caps are usual.

### Indicative values for maximum bridgeable gaps:

b [mm]	5	10	15	20	30	40
s [mm]	0,4	0,6	0,8	1,0	1,2	1,3

Gap width s is the average gap as shown in the illustration.



When new, the gap should be as narrow as possible. The specified fit tolerance can be used as an indicator. The selection and model is left to the equipment manufacturer.

Diameter $d_2$	Fit tolerance $d_G/d_V$
$d_2 < 500 \text{ mm}$	D9/h8
$d_2 > 500 \text{ mm}$	E8/h8

The cover plate can be tilted by  $1^\circ$  or  $2^\circ$  as shown in the illustration, for ease of fitting.

Cover plate gaskets have a rectangular or an internally (less often, externally) sloped cross-section. There is a range of profiles in seven different shapes available, with which all sealing problems can be solved. The necessary deformation to conform to the sealing surfaces is achieved with the cover tensioning bolts.

When laying out the bolts, attention should also be paid to the weight of the cover and where it is to be installed. Depending on the type of profile and the geometry of the gasket, achieving sufficient deformation will require the correct level of surface pressure and/or the correct internal pressure.

The minimum pressure required for a self-sealing connection is given as  $p_{krit}$ . Where  $d_1$ =internal diameter and  $d_2$ = external diameter of the gasket, and the sealing factor is K, the following is true:

$$p_{krit} = K \cdot \left( 1 - \frac{d_1}{d_2} \right) \text{ [N/mm}^2\text{]}$$

The sealing factor K was established in tests and can be taken from the table on the following page.

The maximum permitted operating or test pressure can also be estimated from the critical pressure. The selected tolerances and the presence or absence of metal caps or lathed protective caps is of critical importance.

### The following gives an indication:

Pressure	Model
$p_{max} < 3 \cdot p_{krit}$	without caps
$3 \cdot p_{krit} < p_{max} < 6 \cdot p_{krit}$	with metal caps
$6 \cdot p_{krit} < p_{max} < 12 \cdot p_{krit}$	with lathed steel cap

## Cover plate gaskets

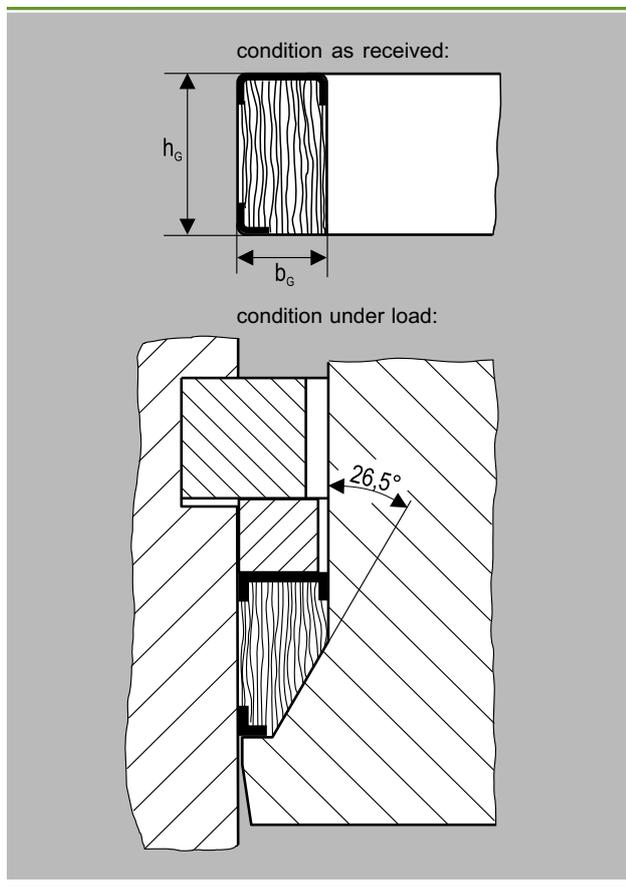
Construction and material of the gasket								R <sub>z</sub> * [μm]
Graphite ring, <b>Profile series P70</b> made from chemically pure graphite, "RivaTherm"	P71	P71K	P71KL	P74	P74K	P75	P75K	12,5 to 25
Factor K (N/mm <sup>2</sup> )	100	110	90	70	80	70	80	

Material for the caps: Stainless steel sheet metal 1.4541 and/or by arrangement

\* Recommended maximum roughness depth of the flange surfaces

1) In packing sets of two or more rings, the intermediate caps can be done away with, please specify when ordering.

### Profile P71KL



The pretensioning force  $F_{sv}$ , which produces sufficient sealing surface pressure, can generally be represented as:

$$F_{sv} = \frac{d_2^2 \pi}{4} \frac{p_{krit}}{2}$$

Depending on the mode of operation, smaller or greater pretensioning forces can be indicated.

The P71KL model with U-shaped and L-shaped sheet metal cap or lathed steel cap has proven to be particularly good for sealing at high pressures. The cover has a slant of 26.5°, which extends to half of the sealing height. When fitted, the sealing ring is shaped into the slanted shape of the sealing space, generally giving approx. 12% radial compression.

The advantage is that all sealing gaps required by the design, into which the graphite could be extruded, are closed off by the caps.

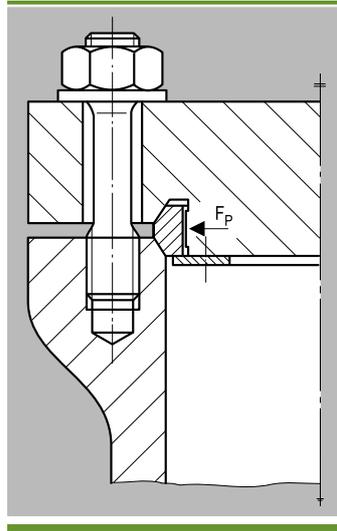
The P71KL sealing ring combines the advantages of a sloped ring, i.e. low pre-deformative forces with the advantages of a plain compression ring, being easy to remove, particularly at high pressures and with large diameters.

Equipment with  $d_2 = 720$  mm diameter and 770 bar test pressure will run perfectly satisfactorily. Larger diameters of more than 1000 mm are used at approx. 500 bar and are just one further example of thousands of safely installed cover gaskets. To achieve an optimal seal  $h_G$  should be =  $2 \cdot b_G$ .

All rings are compressed in moulds. Our extensive range includes tools from a few millimetres to more than 1000 mm in diameter. As the moulds and tools are constantly being updated, an up-to-date list cannot be given here. We would be happy to advise whether a tool is available for the required measurement or whether it would cost extra.

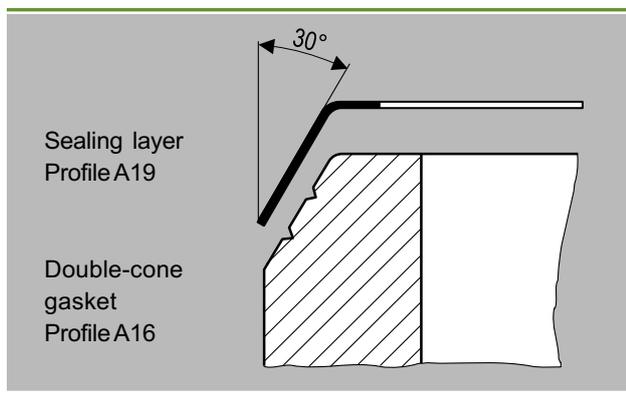
## Double-cone gaskets

Double-cone gaskets are radially compressed like a circular spring by the bolt pre-tensioning force. A pre-tensioning of approximately 1/3 to 1/5 of the test pressure is generally sufficient to achieve the necessary initial seal. So that the gasket does not become overloaded, only a limited amount of clearance should be left between the cover and the gasket. After pre-tensioning the gasket will initially have contact inside to the cover. With the application of pressure it will then spring back by the compressed amount and if there is sufficient internal pressure will expand elastically, so that it offers reliable sealing in all operating conditions due to its optimal design shape.



We would be happy to carry out a cost-efficient check for tracking and to determine the measurements of the double-cone gasket as part of our gasket estimate service. The illustration above show the design principle.

The measurements of double-cone gaskets are not standardised. We can currently supply sealing rings up to  $\varnothing$  3200 mm. The sealing surfaces are conical surfaces with a sloping angle  $\alpha$ . A sloping angle of  $\alpha = 30^\circ$  is usual, but is not suitable in every case.



There are frequently two or three grooves of a few millimetres wide and a few tenths of a millimetre deep on each conical surface. The grooves fix the enclosed sealing layers into position. The layers provide a better initial sealing behaviour.

The sealing layers should be no thicker than 1 mm. Aluminium, copper, nickel and silver layers from 0.5 mm to 1 mm in thickness have proven successful.

If the sealing layers can no longer be produced in one piece from the semi-finished product, they will be welded. The thickness of the welded joint deviates from the layer thickness by between +0.1 mm to -0.05 mm.

Profile AR16 has convex sealing surfaces. The convex model has proven particularly reliable where the strains and curvatures of the component vary greatly, where layers of soft metal are not suitable.

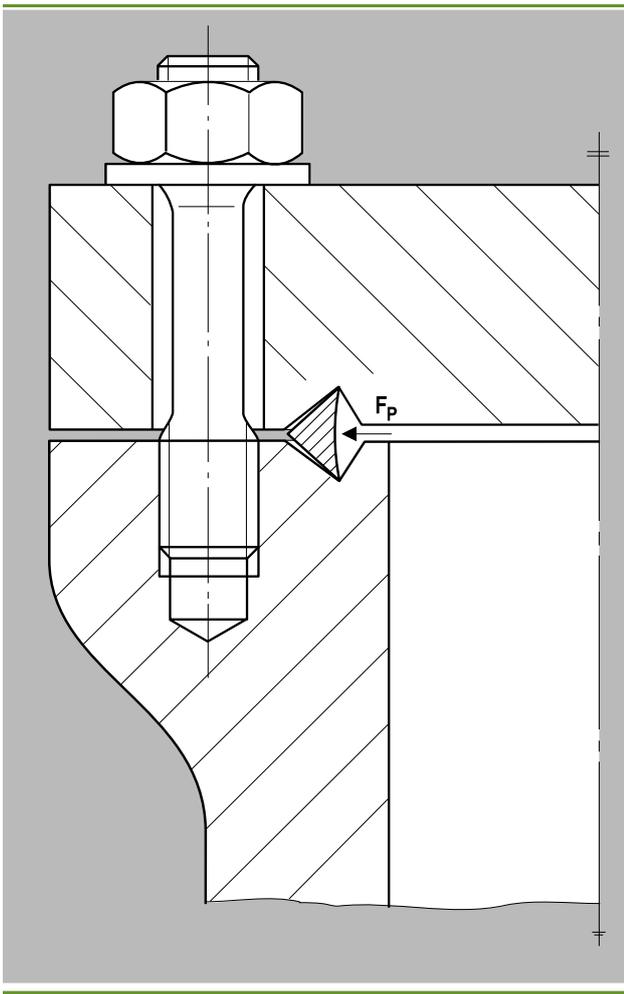
### Gasket profiles

Profile	Cross-section	Material	$k_0$ [mm]	$k_1$ [mm]	$R_z^*$ [ $\mu$ m]
A16		Steel	-	-	1,6 bis 3,2
AR16		Steel	-	-	
A19		Cu, Ni,	$b_D$	$b_D+5$	3,2 bis 6,3
		Al, Ag			6,3 bis 12,5

\* Recommended maximum roughness of the flange surfaces.

## Delta gaskets

Because of their geometric shape, delta gaskets require a higher level of precision from the seal grooves. As a direct result of the manufacturing process and its resulting precision, delta gaskets are only used for high-pressure autoclaves and high-pressure connections up to a maximum of 2000 mm, whereby the majority are less than 1000 mm. The following illustration shows the application as a cover gasket.



Due to its splined profile, an excellent initial seal is created by the partial plastic deformation of the opposing peaks of the gasket when bolt pre-tensioning force is applied. The radially self-sealing effect arises due to the high internal pressure resulting from the elastic extension of the gasket.

Delta gaskets are not suitable for dealing with intermittent pressures. Additional sealing layers are not practical or necessary. Delta gaskets are generally produced from seamless rings. The sealing material should be softer than the flange material if at all possible. Care should be taken to ensure adequate creep strength in the material. The gasket

is only slightly higher than the sum of the seal groove depths, therefore if the grooves are reworked at any stage a new gasket with greater height will be required.

We produce delta gaskets according to your documentation, from all usual materials. See also the section "Materials commonly used".

### Gasket profiles

Profile	Cross-section	Material	$k_0$ [mm]	$k_1$ [mm]	$R_z^*$ [ $\mu\text{m}$ ]
A15		Steel	-	-	1,6 bis 3,2

\* Recommended maximum roughness of the flange surfaces.